UNIT 1 BASICS OF SURVEYING 6105-3 => Definition / ofor ware ! painciples of surveying => (local alline => classification of susveying.)~ (notices or jui) => painciples of chain surveying. Methods of measuring horizontal & slope distance Ranging Wostking of poismatic compass => Types of bearing. =7 declination. -> Dip, Local attraction. => planetable susveying, ESJOJ3. => chain surviva paismatic comprus M Detinition :-It is an ast of determing relative possition on the easth surface by means of horizontal and vertical distance, and hostizental and vertical angles patriciple of surveying :-I Working from whole to part 2. To locate New station by attest two measurements from fixed reference points. classification of susveying:-1 potimary dassification b. Geotic Surveying without come 2250

Elevation - angle base Secondary classification:-(a) Based on pappase: -(1) Geological susveying (") mine surveying (1) Archag Archaeological susveying (1) military surveying (D) Based on field [Mature of field] :-(i) land survey (P) Hydrological sciency (er based on methods survey, curre () Totangulation - where the area is to be subwey is divided (ii) Traversing. in to Network of taiongles It is in the form of circute survey lines which may be open (or) closed Based on instruments :-(i) chain Busivey _ wood (17) compass survey angular marson plane table scenney -> graphical restrict (iv) Theodilate Sustay - Expet angle measurement (a) Tacheometry Survey It is an special type where H, V distance (b) levelling Survey To the determined, indiredly (b) levelling survey To determine the clivations (V) Epril - Electronic Distance measurement (a) T. S - Total station (b) D. G. P. S - Differential global possition system (c) lidas and is used in monominates with in it (c) photo grammetric Survey (iii) plane table survey ? It is an graphical method By which points are plotted on the paper

Seale :-It is an fixed sodio that every distance on the plane which coursesponding distance on the ground Type's of scode's :-U) plain Scale - linear measurements (2) diagonal scale - concentration of yords and leads are ((3.) Vernier scale - least court based on angle. (4) scale of chords Expotencies - + identifiegue (1000) pounciples et chain sussiverying :-*The main participle of chain survey is to be provide frame work which consists of number of well condition taingles. * The triangle is to be well condition which contains angle smalles then 30° and angle grater than no >120 Types of chains;-1 metric chain - som some in Gunter chain _ 3. Engineesing chain - op in Revenew chain - mail of the company dialo 4. Steel chain - For man Instruments et chain survey :-1. choin 2. Tape 3. Ranging stods 4. offset Jods 5. pegy Cross staff -> shout offset 6. optical square > more accuracy - long offset 1. 8 Arrows 9 plumbob

ERRORS in chaining :-(Instaumental errors , Instrument defers (2) Observational Errors (a) gross EJUOUS -> careless ness, blunder mistake [without have ne (b) Systematic ESUIDS -> Anothematic Cryon (c) accendital EJIJIOJ. -> due to human defect Slangow Eziziozi correction to be applied :-(a) Type's -> length correction Tempestature correction >> pur correction > Say correction => slope correction Error: - measured value - true value correction: - True value - measured value bsevet + measur I length correction :- correct distance = (-) x measured distance distance L' = actual incorrect length of chain L = length distinated length of chain Temperature correction: changes in temperature 20 $C_t = \chi (T_m - T_o) \chi L$ d = coefficient of thermal expassion In = mean temperature during the measurement To = Standard temperature L = measured distance

(5) put correction:

$$C_{P} = \begin{pmatrix} P - P_{O} \\ AE \end{pmatrix} \times L$$

$$P = put a pplyed during the measurement
$$P_{O} = standard put
L = measured length
$$A = cross section area
E = camps matter of clasticity
(7) Sog correction:
$$C_{S} = \frac{LW^{2}}{24RP^{2}}$$

$$L = dectinated length
$$P = put applyed$$

$$W = rotat weight of tape
$$N = Atumbers of Equal Backs-(on span)$$
(8) elope correction:

$$C_{S} = \frac{h^{2}}{2L}$$
If O is given then $C_{S} = L(L - cosO)$

$$V_{M}^{M}$$

$$Paintsen := Sitt
Sam steel tape was standardized on a flat ground
at a temperature of Soic under the put of 15kg.
The tape was used in caterary, at the temperature
of 30'c undors the put of long. The C_{IS} area of
a Tape is 22mm and total weight is togoms. the
Coungs module and caelfbeart of thermal expansion the
the steel tape is 91000 kg/mm^{2} and it xito $\frac{C_{I}}{C_{I}}$

$$C_{I} H is 5cm then what is the slope correction$$$$$$$$$$$$$$

Given :-
Length - 20m

$$T_0 = 20^{\circ}C$$

 $T_m = 30^{\circ}C$
 $P_0 = 15 keg$
 $P = 10 kg$
 $A = 22 mm^{-1}$
 $w = 2 loograms - 0.4 kg$
 $d = 11 \times 10^{-6}$
 $E = 21000 kg/mm^{-1}$
 $h = 5am = 0.5$
(5) correction for temperature :-
 $C_{t} = d (T_m - T_0) \times L$
 $= 11 \times 10^{-6} (30 - 20) \times 20$
 $= 2.2 \times 10^{-3} - 3$
 $= \frac{10 \times 10^{-6}}{AE})L$
 $C_{t} = \frac{p - P_{0}}{AE})L$
 $C_{t} = \frac{10 - 15}{22 \times 21000} \times 20$
 $= -0.000246$
(1) Correction for sum
 $C_{t} = \frac{h^{-1}}{2L}$
 $= \frac{20 \times 10^{-3}}{24 \times 10^{-5}}$
 $= 20 \times 10^{-5}$
 $= -0.001324$

= 0.825 = 6.25×10-5 = 0.000063

Total correction =
$$c_{1} + c_{p} - c_{s} + s_{r}$$

= $0.0022 - 0.000216 - 0.00133 + 0.0000-6$
= $0.625m$

Total length = 20+0.625= 20.625m]

D

Gaven :-

A line was measured with a steel tape som at 25° and Pull of 15 kg the tempesiature dusting the measurement was 35° c and pull applyed 25 kg. Assuming Tape to be Supposited at Every 30m, calculate True length, If 9's thema a. 020 m², co-effectant of thesimal symptom 3×10⁻⁶, moduly of classicity 2.1×10⁶ the weight of total matescal 0.8 kg.

$$Length = 30m$$

$$T_0 = 25^{\circ}C$$

$$P_0 = 15 kg$$

$$T_m = 35^{\circ}C$$

$$P = 25kg$$

$$A = 0.020m^2$$

$$d = 3x10^{-6}$$

$$E = 2.1x10^{-6}$$

$$W = 0.8kg$$

(?) correction for temperature ;- $Ct = \chi (Tm - 70) \chi L$

$$= 3 \times 10^{-6} (35 - 25^{\circ}) \times 30$$

= $[0.000900]$

(2) Corvection for pull :

$$C_{S} = \left(\frac{p - P_{0}}{AE}\right) \times L$$

$$= \left(\frac{2S - 15}{0.020 \times 2.1 \times 10^{6}}\right) \times 3L$$

$$= \left(\frac{20011400}{100}\right)$$
(3) Correction for sag:

$$= \frac{Lw^{2}}{241 \times 10^{5} \times p^{2}}$$

$$= \frac{30 \times (0.8)^{5}}{241 \times 100}$$

$$= \left(0.00128 \text{ m}\right)$$

Total correction 1.

0.000900 + 0.00714 - 0.00120

= 0.0067

$$\frac{10^{1}a!}{= 30.006m}$$

A steal tape 20m long standastidized at 55°C with a pull of 10°kg, find arrection for Tape length if Temperal use at the Time of measurement is 80°C, weight of the tape 0.8Kg and area 0.051 cm², coefficient of Expansion G2 x10⁻⁶ Elasticity is 2.109 x10⁶ kg/cm² pull Extraked \$1 [6/kg length = 20 To = 55°C Po = 10 Lg

$$Tm = 80° C$$

$$P = 16kg$$

$$w = 0.8 kg$$

$$w = 6.2 \times 10^{-6}$$

$$E = 2.109 \times 106$$

$$A = 0.051 \text{ cm}^{-1}$$

$$C \text{ correction for for put }$$

$$= 6.2 \times 10^{-6} (80 - 55) \times 20$$

$$= 0.003 \text{ lm}$$

$$C \text{ correction for put }$$

$$C = \left[\frac{P - P_0}{AE}\right] \times L$$

$$= \left[\frac{16 - 10}{0.051 \times 2.109 \times 10^{6}}\right] \times 20$$

$$= 0.001 \text{ lm}$$

$$C = \frac{Lw^{-1}}{2405 \times P}$$

$$= 20 \times 10.8)^{-1}$$

$$20 \times 10^{-8}$$

psismatic compass:principle of compass surreying :-The painciple of compass scarreying is traversing which involves services of connected lines wosking of prismatic compass:-The working of possmatic compass involves the following steps centering ; - leveling, observing the bearing Types of beasings :-"Types of mesuidian:messidian is a standard disaction from which bearing, of scenney lines are measured There are three types of meridians. 1. True mexidian - Lisrup and and such control posted 2. magnetic mestidian = 1 3. astbitasy messidian Et is convinent direction Assumed this mestation by more using of bearings? beasing :-It is an hostizontal angle made by survey lines with relevance to mestidian Type The orgie marks will interven to the 1 True beasing meridian is and the terrary later and history histor 2 magnetic beasing the right with relation of the relation of - 16 g c l'increa la patiatory menulari i a una dura l'un



$$(a) (B = 360^{\circ} - wc)^{\circ}$$

= 360^{\circ} - 303^{\circ}

= 180 - 109-

=STIE

2	convert Reduced Bearing in to whole cisicle bearing
75	(9) AL 52:30'E (NE) 16.10 A 52'30' 1019
	e) 5 36 15 E (sc)
	C'SBr 4r' W (Sw)
	e) N 15' 10' 10 (NW) Sign' NO. LOCK
	130 B. 17 30141
	(a) web = acb
	= N 5230'
	(b) S 30 15' et
	RB= 180-WCB
	$= 180 - 30^{\circ}15^{\circ}$
0L	= 149°.45'
	(C) \$B = WCB + 186
	= 25"4611100
	5 205 45
	(d) RB = 360 - wcB
	= 360 - 15'10'
	= 344° 50' all 8 and publication all all a
	local attraction:
	Local attraction in
	the also known as Exister Value.
	the compass needle is affected by presence of image
	and steel Such as electric abie
1	they will deflect the liter capies steel gladeas E.I.C.
	effect is known as needle and this distubance
	Fre la local attraction
行	use bearing and back bearing.
	tope bearing:
	Fore beasing is a line measuring former land
	Survey lines

1		1		
	<i>(</i>)	× S E		
	L	B S		
	A			
	5			
Reach (Penting !			
and t	second -	is a line	meaning for	noand
Back	Beasing	10 - 20 6	head Back Ba	nº01
back	wand di	rection is co	und balle ad	stirg
	K-H	noul Cryb		
O The) nunuting &	observed in	traversing	with compast
Inhere	local	Htraction is	suspended f:	1 amount
Nº of loc	ral otta	ction. at diff	erect station	s correct
the b	eastina 5	flines and	inclined angle	s
	g		Ø	
	Line	FB	BB	
lor a'	AB	59 00'	239'0'	
	ВС	139°30'	317 0'	
	CD	215 15	36:30'	
	DE	208 0'	19'0'	
	EA	318'30'	138 45	
XXXX				
Noto:-	The differ	aence between	n n	
fore be	axing and	I back bearing		
of sue	wallnes	should be		
Equal	to BRO		* :	
	100			
Solution	2			
The	1.			
Inc	line AB	ra Pla		
Be	5 0-1 BA.	TH TO UT		
5	239 0'-	Saco' NO	correction of A)	
~	1800			

Be line EA FB of EA - F.B of AE = 138' 45' - 318' 30'= -179' 45'Adding The line EA = FB of EA - BB of EA = 318' 30' - 138' 45'

= 174' 45'

- 114 45
- = 180° -129 45'
- = 0 15

Here 0'15' Correction at "E"

Re line DE

- = Actual + correction
- = 200' +015'
- = 2915
- = F.B of DE B. O of ED

- 1

- = 208'0' 2919'
- = 178'45'
- = 180 -178 45'
- = 1'15'

Here i's correction at D

The line CD

- = Actual + correction
- = 36°30' + 115'
- = 3\$° 45°

= F.B of CP - B.B of DC = 215 15 - 3745 + 111° 30' = 180- 171'30' = 2° 30', Here 2°30' correction at C · 10 (al Re line BC = Actual + correction = 317' 0' + 2'30'= 319 30' = B.B of BC - F.B of CB = 319 30' - 13 a 30' = VX1/818 = 1800 = 1810 - 11730 Total corrections A =0, B=0 7 2/80, C= 2° 30' +D= 11+1 Here al the confection at B 1) Forgen by = 2'30'+115'+015' Vive AB ve 7 Actual 10109 25-400 · local attraction is 4'0'0" 180-180. Write following beasings where obsessined while A= 00 Traversing with compass B= -25' # B B.B Line 45:45' (A) O 22.6.10 CB) AB

9.6: 55! (B) () (C) ~ BC CD 29 45'(0) DF 144 48' 3240 421

2.26 00 \$ (-25')

+-209 10' (D)

Alt is a poer open traversing.

observed bearing beasing corrected Line Correction 45 45' (P AB NO correction as A 45.481 Lister (435 come) BA 226 10' 22610-225 451 - 1125 -0'25'00" BC 96 55' 96 30 271 5'-96 TO -0'21' CR 279 5' -30' 27630 CD 29 45' -351 29'10' DC 209'10' No correction at 020 209° 10' DE 324 48' wo correction at p >0 824 481 ED 144 48' No correction at E=0 144 48'

It it is open traveruse Assume Correction as

Stort Andreas

A = 0°

1.61 . 61

· · /,

B completed.

C = -35' error

A = \$\$ Assuming a 18 a 20510

line	F.B	B.B
AB	44° 40 (N)	223°20' (P.)
BC	96°20' (B)	274" 18 10
CD	30' 40' (C)	212"2" D
PE	320 121 (D)	140 12 5

Assuming A 15 a 20510

1

~

Line	obsestived bearing	correction	Corrected beauting
AB	44 40'	No correction as A	44° 40'
BA	225 201		an a
BC	96 20'	- 0 G -	2.5 200 . 4
CB	27 4 18	2° 2.2.	575 LIO 1
CD	30'401	1.5 2 4.1	32 2
DC	212° 20	NO Correction	212" 21
DE	320121	NO Correction	20.51
ED	140121	at D=0 No Correction	

3 1

2711 18'- 95 40'

17838 120 - 11839 1 221

closed Traverse problems

1-

intervice or p below 160

: Exterior ma

i seco

above 120

10.00		DR
une	FB	B,D
AB	75'5'	254 20'
BC	ils° 20'	296 351
CD	165 85)	845 3 5
DE	224 50	
Et		44 5
	804 50	125 5

No Grron at C.D = 180=18 20

105-5-1155

- + 0 20

There is NO correction in Cand D

Line	observed	Corre ction	corrected beasing
AB	75°5' ()	o 30)	75 359 24
BA	274 20	1' 15	255.00
Bc	115 20	12 1 5	1,6,35
CB	296°351	No Correction	296.201
CD	165 35	at 'c'	11 225
DC	2	at c'	165 35 ! 9 18
) E	345 35'	No Correction	345 36
D	(r, r);	org D wo connection	224 501
A	30430	-0 451	44'su' al E
F		ل در ۲	305' 35' at F
	رته که د.۱	0 30	12535 at A

ale iou acaria O following Bearings are taken at closed toverse and land Line F.B B.B AB 259 0' 61 86 10' (A) BC 120°20' (B) 801 50' C' 10 Ca the CD 110 20' (350' 50' ?) 0 £ 230 10' (D) 49'30' 13 0 15 (1) 310 20' (E) EΔ compute interior angles and correct them with blowing Easons, At angle LA = B.B of AE - F.B. of AB. = 13015 - 8010' = 50'5' At angle LB = B.B. of BA - F.B. of BC = 279°0' - 120' 20' = 138 40' At angle LE = B. B of - CB - F B of CD = 30150 - 170 50 = 1310' = B. B. P pc - F. B of DE At angle LD = 36° 50' - 23° 10' = 120 40' At angle LE = B.B. of ED - F. B of EST = 49 50' - 310 20'

- = -26° 50'
- = 380' 260' 50'
- = 99'10'

Ø

compute the intestion angles
LA = B. B of AFE - F.B of AB
$= 22^{2} - 45^{2} - 105^{2}$ = $303^{2} - 105^{2} - 15^{2}$
$L^{A} = 19730' = 350 - 19730' = 162'20'$
LB = B. B of BA - F. B of BC
- 285 15 - 2001
$LB = 265^{\circ}1' - 360^{\circ} = 94^{\circ}45'$
LC = B. B of CB = E.B of CD
= 200 0 - 229 30
= 0+29°30' 1 to to 8.8 - 4-14 91
D = B. B of PCE + F. B of PE
= 4980' - 185'19'
= + 137 45'
LE = B, B, F ED - F. B of EA
$= 7'_{15}' - 122'_{45}'$
= 115' 30'
$check = (2n - u)q_{0} = (4 + (B + Lc + L) + LF)$
$(2\times5+4)q^{0} = \frac{147350'}{162'30' + 94''45' + 29''80'}$
+ 137'45'+ 115' 30'
$540^{\circ} = 540^{\circ}$

Recination:-

. The Declination at the plane is hoursontal angle between true meridian and magnetic meridian It is known as declanation

- ? Il magnetic messidian is at right susside [East side of true messidian] Then the declination is soud to be positive
- 3. If It is at (west side) of true meridian that

is soud to be negative. De magnetic n - og i sta - t g \$ 63 1: (也):)] "

e Si kewith the state of the prodem

O The following bearing is taken on a closed compar

tagverse, n Damis on the

ochrantine hast budgeness and time AB

BC 170' 50' 350 50' - 180' CD

DE 230' 10' 0 49' 30'

EA 310 20' 130 15' 108 8 8 B ..

at what station do a you suspect local attraction. determine connect magnetice bearing it declination was 5 10' E then what is the true bearing

l	ine	obsesta	d Correction	corrected	NLE	Bearing	12 mails
	AB.	80' 10'	45 0+	80 05 30	in 86	5	
	BA	25901	1 57 68	26055'	266	s'.	
	Bc	12020'	159'QB	122 15' 1	127'1	5	. e
unnissi	CB.	301 501	o Q C	301 50'	301		
	CD	178 50'	U Q C	ואל ליכו	501		· ·
Hhe	00	850 50	000	1350 50'	s od	14	
	DE	230 10	0 QD	236 (0'	3560	būsā M	0
	ØD	4a 301	40° @ €	51.1	233	1	
	EA	31 v 20'	wor	2110/	55 20		
	AE	150 181	4504	131 0	816 10'	,	
The fi luca B.B magi	aversisi aversisi and and	ing with thraction True direction	F.B and n q Con is sus Bearing n 10°60.	B.B where pass in H spected fir	obses ne p nd c lines.	ined in lace iorreck Given	He where d -f. Bon that
	0.0		50	50 350	1 or		

line

49' 30' 88'30'A) Q19" 15 B, 02 012 AB Be loo 45 to une 30's nother CD 25 45 mind 2011 15 Bar burn,

DE 320'10' Maisin' port

Line	obseawed	Correction	Corrected	True Bearing	j Romark
AB	38° 30'	1'30'6 A	400-10	3001	
84	219'15'	6 45 65	220 0'	2,10 0	
BC	100 45	0 44 00	10 30'	`a'r 30'	Remain
cB	27830	1' 30' atc	280 0'	870	A; I, C
CD	25 45	1' 3d at C	27'15'	ຕ ເຈົ່	Affected
DC	201 15'	0 @ D	Q01'15'	191 15'	601-1A
DE	32510	0 @ D	82515	315 15'	
ED	141'10	0 QE	145°10'	135 101	

2) Dipi- Rip is also known as magnetic forcunation 2 The magnetic inclination is an angle made with hoseizontal by caseth magnetic field lines. 3 These lines lies in different points on easth Starface CONTRACT OF STATES Ranging 18 known as method of locating by Establishing intermediate points on a strught line banging :between two fixed points there are two types of Ranging 1 Direct ranging ? Indirect stanging NO Proplane table Susneying It is an graphical method by which proto are plotled on the paper

Apparatus 1. Sport level

2. Alidade cipital surchas 4 plumbing tostemain représented the point on the print 5. plane table 3. Trough comass 5. plane table 6. Tape 6 TI wind get a grurate 2 Ranging sids handling is vory 1 ugs 1 ERADAS :-C 1 1 2 3 1- Instaumental Error 1 16 10 2 Sighting Error 1 де 👌 🖉 🧎 Э The state of a r plotting Garaions antimethods of plane bable: -- Lab 1 sadsation provethod 2 Intersecting method while ye betractional 3. Traverse method while a set that set is 4. resecting method (a) Two point resecting problem (b) Three point problem stand final and points Bulling reaching and ran in paipar : + ra. Millaren to parts a an an an a

UNIT: 2

THEODOLITE SURVEYING

levening

Basic Definations
Types of levelus
Types of leveling states
Temposiasy adjustment
Methods of leveling.
Las Hight of instrument
Rise and fau
C: Effects of curvacture and Petriaction
Revelling: - It deads with determination, of clevation of points.

Matur line: - Referance line Any surface to which elevations are referred is known as daturn. mean sea sevel:-

The average height of sea at all the storges of tides at several places.

Elevation :-

Elevation is a point by which restical distance of a point above and below the sustance of Easth

Bench masik :- It is an relative permanent point

line of reference with respective datum Types of Bench masis :-501.91 1) GTS (great trigrometric survey) 2) pwp he nent benchmasik 3) Temposlazy bench masik India BM is in Muron 4) Ostbatesly bench masik GIS - It is Getablished by Suzvey India at a intervel of 100 km all over the Conuntary mumber posil "It'lle" he Poron permanent benck masik:-It is established between Grs bench mark govenment agencies like By the puop [public woosiles department These points are located at stations points and kilometer stones wall of buildges Tempozazy bonch mark :-It is a Referance point on which day work is closed and continued for next day. Asbotasy bench masure: It is an Assumed bench mark tox small leveling tose sight :-It is last sight taken before moving the Instaument. Back sight: first sight taken after setting of the It is a Instrument

Types of levels :-1 Dumphy level & wye los y level 3. Tilting level 9. Auto level. Dumphy level :-It is an simple and compact installment, Telescope is signally (fixed) to its supports. where NO Jotations. Tilting level Tritting level is also known as Indian office pattaan. In this telescope is slightly tiltled (moment y tenel :-It is a combination of blamphy level and filthing level. In This telescope is zotaled and moved and Jused. Auto level :-It is a self alignning instrument die to presende of compensation device [prusm] Types of leveling staff:-1, self reading leveling statt (ranged) 2 Target levelling staff ----a oxdinaxy staff sign show in height Self seading :fording staff -2m b. stop with telescopic staff C, yoron 191 Used aver

Temposiasy Adjustments of level 1. setting up the level, leg rainstment levelling up foot scours regulation 2 3. Elemination of pascallax _ coops bro Zin · Adjustment in Instaument Methods of levellings which used the plemospheric presive 1. Brownetric levelling and distance 2 Trignometric levelling - indirectivered angle toam mo 3 Sport levening - hoursonlat live on basin a skar : . 12 (n 11 - n Attrisiphesite pressure & to /H IFF & and D, values is known basic sudes are applyed [sine such cossel] and we find the height (a) Simple levelling by differential levelling, (a) thy levelling charge at interment in den profile leveurng - wishing ingil i long (c) precise levelling the result of the strong the stro Kille. Gir .r. .81 m determination of levelling :-· Pul 1. tro 4 +1 I - Hight of Instrument file and face method

Hight of Instrument:-HI = B. S + R.L RI = HI - FSON IS - Intermidiate sight Hight of instrument is also called collimation paoblem :-

The tonowing staff readings where observed Successfully with level of instrument having 0.675, 1230, 0.750, 2.565, 2.225, 1.935, 1.835 3.220 3.115 and 2.875. The first staff reading was taken with staff held on bench maxik. with reduced level loom. The Instaument have been shifted After the Second and 5th and 8th reading Enter the readings in

the	level	book	and	find	R.L	of	He	points	
-----	-------	------	-----	------	-----	----	----	--------	--

	5		51-			
Station	B.5	IS	F.S	HI	RL	
	0,615	8.1		100.675	100 051	
	0.750		1 230	09,495+ 0750 = 100.195	99, 454 (1) -	
,		8,565	2011		100.195-2. 565 = 97.630	
	1935		8,825	99,70+	100, 195-2.565 99.970	
		1.835			98.07	
	3.115	N 6 2	3.220	96.685+	99.905-322	
			8.875		96.925	
lect :-	285		2 PS			
	5 BS - 2	c c s = la	stri- ti	rst R L		
	6.475 - 95	50 = 96	921 - 100	5		
	3.015	= 3.0	1121			

Rise and face method :-

1 The following readings where observed successful with levelling Instrument. The Instrument has shifted after 5th and 11th reading 0.585, 1.010, 1.735, 3.295, <u>3.775</u>, 0.350, 1.300, 1.795 2.575, 3.375, <u>3.895</u>, 1.735, 0.635, 1.605.

Draw page of level book and determine RL at various points By which first reading of RL was taken as 135.0.m.

station	n B.S	2. L	F. S	Rise	Fall	RL
A	0.585	-	185 - A1	* , I	100	135.00
ł		1.010	Ĺ		0. 425	1.84, 57
1	1	1. 7.35	1 -		0.725	133.85
- 8		3. 295			1.560	182 290
B	0.350		3. 775		0.480	131.810
	011 -	1.300			0.950	130.86
· · · ·		1.795	694 8		0.495	130.365
e e.º.	init in	2. 375			0.780	129.58
(((6) (-)	ाले तर	3. 375	1.11		0. 800	128.78
C	1.735		3.895		0,520	128.20
		0.635		(. 1 d)		129. 765
	· -	(1.605		0.970	126. 39
	ERI, 9	Eria Par		ERALI	Sri	

Zact

The following readings where observed Successfully with levelling Instrument the Instrument has shifted 6th, 10th 0.680, 1.455, 1.855, 2.330, 3.885, 3.880, 1.055, 1.860, 2.265, 3.540, 0.835, 0.945, 1.530

2.250 , RL was 80.150

Station	B. 5	J.S	F.S	Rie	Fau	R.L
	0.680					80.160
		1.455			0.775	79.975
	1	1.855			0.4	79.575
		2.330			0.475	1.91
		2.885			0.555	18.545
	1.055	*	3.880		0.495	78.05
		1. 860			0. 801	71.245
		2 265			0.405	76.84
	0.835		3.540		1. 275	75.565
		0.945			0.11	75. 455
		1550			0.585	74.87
		2250			0.72	79.15

E85 = 207 Ets - 692 JR = D LOSL # - - - 14 15 5 Bar - 66 1-11- 20 1-Chester -

> SRID-IF - Lail R. - E.X. P. 0-66 - 74:15-30.750 66 - 66 1 1 1 1 1 1 1 1

2.0 Effects of curvature on levelling

1. human Essos

2. Instaumental Earlos

3. Natural Garos

e) cusivature error - Depend on early Instaument has a more delange to there is a form of Estros



It the idistance is less the time of sight ind hospitalitie win be liet on some line Single line

1 (P. 1.

By applying pythogsupes theorem :-

$$(R+G)^{L} = R+d^{L}$$

 $R^{L}+2RC_{c}+C_{c}^{L} = R^{L}+d^{L}$
 $C_{c}(2R+G) = d^{L}$
 $C_{c} = \frac{d^{L}}{2R} = \frac{d^{L}}{2R}$
 $C_{c} is negatible$
 $Refraction:-$
 $C_{R} = Y_{R}C_{c}$
 $C_{R} = \frac{1}{2} \times \frac{d^{L}}{2R}$
 $C_{R} = \frac{1}{2} \times \frac{d^{L}}{2R}$
 $C_{R} = \frac{d^{L}}{14R}$
 $Efore E here present we take - work the
 $L_{x}(N_{c})$ $L_{x}(N_{c})$$

In suse and four method the gradient is gradient: $\frac{\Sigma f_{au}}{L(n-1)}$ nz no. of readings

Included = previous line ± 180 - Next line.

UART 2-2 Count contouring:-=> Definition 1 => uses of contacts => characteristics of contours XXXXX =) methods of contous => Interpolation method 1) detraration. A " heating has a go => prawing of contout · 010 / E- 5 Permit : 1 - 1 - 5 Definition :to satura go Tit is an Imaginasy line on the ground surt. Joining points of Exqual Elivations. Joining lines is known as contown lines A group of contour lines Represents contour map. (this we vices the silver west the Contour Interival :-The vestical distance between any two consecutive contours is called contour Interval (UN) Join It is a difference between RL of two contours is known as contours interval

tivatizant al Equivalant :-

in The hoaizontal distance between any two contours Consedutive Contousis is Called Contour Equivalant

contous gradient :-

The statio between contour Interval and hosizontal Equivalent

use's of contours ;-

1. It is used to calculate capacity of resorrow It is used to calculate slope of drivage

It is used to alkin canaly roads, and statutary lines

It is used to determine gove direction of 4. ground surface

It is estimated quantity of acting and filling 5.

G. It is used to find the possible route of communication between two points.

characteristics of contour (or) properties of contact

1. Two contours lines of different Elevations can cross Gachother in the case of over hanging cliff 2

2. If two contour lines of different clevations Can unite to four a line

hargers -H
In the case of child vestical cliff



- 3. contour lines are close together which indicates steep slope.
- 4. It contours lines apart 1000 [for] which indicates gentle slope.

5 It contours lines with more highers voib RL Values. Inside which represents hill 6. If Rich' contours lines with how more lowers RL values Inside which represents voting Valuey.

7 The contours lines cross with surger line at a slight angle it forms u-shape contours 8 The contour lines cross with valley line at a right angle it forms V-shape contours



10. The contour lines must be close's but annot be with in the limit of map [map scale]

Methods of contours:-

- 1. direct method
- 2. Indirect method

Rived method :-

- 1. In this method R.L. values are joined directly on the field
- 2. This method is suitable in the case of smaller areas.
- 3. It is highly accustacy.
- 4. This method takes more time consumption
- 5 This method is expensive.



Indirect method i-

I In this method contours lines are joined with Veterence to guiding points at is divided in to those types (a) square method (or) coordinate method (s) (b) cross sectional method (s)





position of 605, 615, will be passess through 0, b, c, d.

graphical method:-

In this method the points are plotted based on x-axes



Drawing (or) sketching of contours :-

1. After Interpolation of antocur between the guide points are joined smoothly and it torms smooth Curry 2. while drawing the contour line fundamental properties should be consider, (characteristic)

- 3 contours lines should be Inked with the key of black and barrow colour
- 4. The contour lines for stoads and salway lines should be shown in brown colour.

UNIT: -3.

Areas & volumes

Areas: _ 2 Qualla

Determination of a very consisting Regular Intervals
Determination of avery consisting Intervals
Methods of alculating averagior, computation of aver :1. Dividing total aver in to number of toliangles.
2. Based on offset to the base line.
3. Based on latitudes and depathures directors
4. Based of co-ordinates total station
5. Based on mechanical method. planime less is a reconsidered at the base of the base of the based o

Based or offsets to the base line larger arres,

There are faces sules used for adculating area Based on offsets to the base line.

- 1. Mid-ordinate sule.
- *2. Average (or) manosidenate such
- A#3 Trapezoidal siller
- ##4 Simpson's one thisid rule

Mid-ordinate sule:-

In this succe Base line is divided in to NO. of divisions and ordinates are measured mid point of each division



a_lis + os dar i ... Na 2 × 13.v .

下在

tosmala :-

* refuter

A = dED = 0 = ordinales, sum of mid coordinales d = distance of each divisions



In this method offsets are measured to Each point of division of the base line.

 $A = \frac{L}{n+1} \ge 0 \qquad A = \frac{n-1}{n} \left(0_0 + 0_1 + 0_2 + \dots + 0_n \right) d$

L = Naxd L = kength of base line n = number of divisions. d = distance at Gach division E 0 = Sum of ordinates

3 Trapezoidal Jule:-

In this feele we will assume figures as Trapezade this method is more accurate than the above methods formula:-

 $A = \left(\frac{o_{c} + o_{n}}{2}\right) + o_{1} + o_{2} + o_{3} + \dots + o_{n-1} d$

Simpson's one third state: -

- Note: Simpson's sule is applicable only when Number of ordinates in odd contritions O = ordinates N = Numbers of Andrinates
 - d = distance at Each division

Regulars interval problems(or) Regular boundary problems The fallowing perspondicular offsets where taken gt Every 10m Interval from the survey line two an I rangular boundary line calculate Area between the survey lines at inregular boundary line by applying

U mid osdinate

D

- 1) Average eman ostinate
- (1) Trapezoidal rule
- (v) simpsons duk

3. 25, 5,60, 4.20, 6.65, 8.75, 6.20, 3.25, 4.20, 5.65

(1) mid rule

$$A = d \leq 0$$

= 10 (0, 10, 10, 10, 1 - - + 08)
= 10 (3.25 + 5.60 + 4.20 + 6.65 + 8.75 + 6.20 + 3.25
+ 4.20 + 5.65)
= 417.589.m. wm²

(i) Average Vule

$$n_{2} no . of ordinates = q$$

$$A = \frac{q-1}{q} (3.25 + 5.60, 4.20 + 46.65 + 6.15 + 6.20 + 3.25 + 4.20 + 3.25 + 4.20 + 5.65)$$

$$= 42.44 m^{-1}$$
(ii) trapezoidal Vule

$$A = \frac{q}{2} (0.40n) + x(0.403 + 0.4 + -40n) d$$

$$= \frac{3.25 + 5.65}{2} + x(5.60 + 4.20 + 6.65 + 6.15 + 6.20 + 3.25 + 4.20) + 5.65 + 6.15 + 6.20 + 3.25 + 4.20) + 5.65 + 6.15 + 6.20 + 3.25 + 3.65 + 5.25 + 5.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25 + 3.25$$

Trape roidel rule, Simpion, rule

Jazigulas boundaryes :-

The distance between Each division will not be Same (or) Equal

paoblem s

Op The following pospondicular offsets where taken I'v from chain line to an insigular boundarily. chainage - 0 10 25 42 60 75 offsets: 15.5 36.2 51.8 21.6 29 31.5

Calculate Area between chain line, boundary and Ord offsets by using trapezoidal sule Solution:

Trapezodial rule

 $\Delta = \left(\underbrace{\frac{o_0 + o_0}{2}}_{2} \right) d$ Area $a_1 = \left(\frac{15.5 \cdot 126.2}{2}\right) \times 10 = 208.5 \text{ m}^2$ $B_2 = \left(\frac{26.2 + 31.8}{2}\right) \times 15 = 435 \text{ m}^2$ $\Delta_3 = \left(\frac{31.8 + 26.6}{2}\right) \times 19 = 487.9 \text{m}^2$ $D_{4} = \frac{25.6+29}{2}) \times 18 = 491.4 m^{2}$ $br = \left(\frac{29.431.r}{2}\right) \times 1r = 453.7m^{2}$

Total Area = 0, + 02 + 03 + 04 00 > 2016. (m2

The fou	iowing	peal	pondi	cular	offs	et) u	shore.	la	bdu	056
farm ch Survey 1	ire, b	ine coundas	y an	d G	d of	lset	Бу	usi	ng	
Trapezoic	tal su	ue of	w.do	Smps	1001	rule	20	Trav	110	140
Chainage	0	15	30	45	60	70	80	100		
offsed	160	8.5	۲. סו	12.8	10.6	9.5	8.3	7.9	6.4	44
Od:	= \$5 = 10		•	U						

0 d = 20

 $\frac{Napezoidal}{D_1} = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}{c} 0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}[0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}[0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}[0_0 + 0 \\ 2 \end{array} \right] = \left[\begin{array}$

consider section O

$$\frac{P_{1}}{r} = \begin{bmatrix} 0.469 \\ r \\ 15430445 \end{bmatrix} \times 15 \\ \frac{P_{1}}{r} = \begin{bmatrix} 260410.6 \\ r \\ 1 \end{bmatrix} + 8.5 + 10.7 + 12.8 \end{bmatrix} \times 15$$

$$P_1 = 616.5 \text{ m}^2$$

Consider Section
$$O$$

 $O_1 = \begin{bmatrix} 0.648.3 \\ -2 \end{bmatrix} + 9.5 \end{bmatrix} \times 10$

consider section 3

$$\Delta_3 = \left[\frac{8.314.4}{2} + 7.946.4 \right] \times 20^{10}$$
= 413 m²

. Total Area =
$$P_1 + P_2 + P_3$$

= 616.5+189.5+413
= 1219.02

Simpson's sule:-

Section (1) $= \frac{d}{3} \left[(0_0 + 0_0) + 4 (0_0 + 0_0) + 2 (0_2 + 0_0) \right]$ $= \frac{15}{3} \left[(1.60 + 10.6) + 4 (8.5 + 12.8) + 2 (10.7) \right]$ $= 4386 m^2$ $= 4386 m^2$

Section \mathfrak{O} = $\frac{d}{3} \left[(0, 40 n) + 4(10.6) \right]$ = $\frac{10}{3} \left[(0.6 + 8.3) + 4(9.5) + 2(0) \right]$ = $189_{2}67 \cdot m^{2}$

section 3

Apply this sule form from 1403 = $\frac{20}{3} [(8.3+6.4) + 4(7.9) + 2(00)]$ = $308.61 m^2$

4th ordinate -> 0000 xd

2 108

Total area = 308 67 +108

= 507.67m2 416.6m2 - 33

 $\frac{70 \text{ tal}}{= 6^{2} 4 + 189.64 + 916.6}$ $= 1230.3 \text{ m}^{2}$

Serepsone. 100005 1000

1. determination of volume by using c/sexual level mthod (a) Trapezoidal tormula (b) prismoidial tormula (Simpson) (volume of carth work, cuttings, and embankments] 2. Determination of volume tor barrow pits

Retermination of volume by using cross sectional method.

There are 5 cross setronals are present 4. Level section

& Two level section

3. Three level section

4. side thill two level section

5. Multilevel Section.

level section :-

A = (btnh)h

Here b = width of formation h = depth of formation (or) height from center n = horizontal to I vertical (ground lover)

lin 2 n = 2

level section:

$$A = \left[\underbrace{n \times \left(\frac{b}{b} \right)^2 + m^2 \left(b h + n h^2 \right)}_{\left(m^2 - n^2 \right)} \right]$$

Here

m = Horizontal distance to I vertical

[Inclined condition]

Three - level section :-

$$A = \left[\frac{b}{a}(h_1 + h_2) + \frac{h}{2}(\omega_1 + \omega_2)\right]$$

to the sec

hi, hz = side heights. w, w_ = side width

For calculating volume at caoss section Level method we have two formula 1. Trapezoidal formula $\Psi = d \left[\frac{A_1 + A_0}{2} + A_2 + A_3 + \dots + A_{n_1} \right]$

2 paismoidal formula $V = \frac{d}{3} \left[A_{A_{n}} + 4 \left(A_{2} + A_{u} + A_{6} + - - \right) + 2 \left(A_{3} + A_{5} + A_{7} + A_{7} \right) \right]$

paoblems

O The postsmotidad Railway Embankment Iom width with side slope 11/2 ton Assume ground is to be levelled in a direction to a center line with Calculate volume in a length of 120m, the centre height at 20m Interval being 2.2, 3.7, 3.6, 4.0, 3.8, 2.8 2.5 Given, width of formation b) = 10m side slope = 142:1 the in the new n=1.5 Total length = 120m. Interval = 20m. Same level A = (b + nh) h $A_1 = (b+nxh_1)h_1 = (10+1.5xe_2)2.2 = 29.26m^2$ A2 = (10+1.5x3.7)3.7 = 57.53 m2 A3 = (10+1.5x3.8)3.8 = 59.66 m2 Ay = (10+1.5x4.0)4.0 = 64m2 AS = (10+1.5x 3.8) 3.8 = 59.66m A6 = (10+1.5×2.8) 28 - 39.76m A1 2 (1011.9×2.0) 2.5 = 34.37 m² Trapesoidal V= d [A 1+An + Az + As + Aa + As + As + As + As 7 $= 20 \left[\frac{29.26+34.37}{2} + 57.53 + 59.664 64 + 59.66 + 59.76 \right]$

17437

prismoidal

D

$$V = \frac{d}{3} (A_{1} + A_{n}) + u (o_{2} + o_{4} + o_{6} + -) + 2 (o_{3} + o_{8} + -1)$$

$$= \frac{20}{3} [(A_{1} + A_{n}) + u (A_{2} + A_{4} + A_{6}) + 2 (A_{3} + A_{5})]$$

$$= \frac{20}{3} [(Bq + 34.51) + u (57.53) + 6u + 36.7) + 12 (57.64)$$

$$= \frac{20}{3} [(Bq + 34.51) + u (57.53) + 6u + 36.7) + 12 (57.64)$$

$$= \frac{20}{3} [(Bq + 34.51) + (57.53) + 6u + 36.7) + 12 (57.64)$$

$$= \frac{20}{3} [(Bq + 34.51) + (57.53) + 6u + 36.7) + 12 (57.64)$$

$$= \frac{20}{3} [(Bq + 34.51) + (57.53) + 6u + 36.7) + 12 (57.64)$$

$$= \frac{20}{3} [(Bq + 34.51) + (57.53) + 6u + 36.7) + 12 (57.64)$$

$$= \frac{20}{3} [(Bq + 34.51) + (57.53) + 6u + 36.7) + 12 (57.64)$$

the stailway embankment 400m long 12m wide at any formation level, it has side slope 221. The ground level at every 100m along the central line as follows. The formation level at ochangy is 207. and Embankment has staising gradient line 100. The ground is level across contral line calculate the volume of Earth work.

Distance 0 100 200 300 400

400

RL 204.8 206.2 207.5 207.2 208.3

Given,

b = 12 m n = 2 h = 3 total = 400m

Distane	R.L	formation	dep ty a se sa		
0	204,8	207, 0 tinioo	207.		
100	206 L	208	208-2062		
200	201.5	209	15		
300	207.2	210	L D (-		
400	208.3	215	26		

$$\begin{aligned} \frac{12 \text{ kel}}{A \text{ req}} & = \underbrace{12 + 2 \times 2.2}_{2.2} = 36.08 \text{ m}^2 \\ A_1 = \underbrace{(12 + 2 \times 2.2)_{2.2}}_{2.2} = 36.08 \text{ m}^2 \\ A_2 = \underbrace{(12 + 2 \times 1.8)_{1.8}}_{2.5} = 28.08 \text{ m}^2 \\ A_3 = \underbrace{(12 + 2 \times 1.5)_{1.5}}_{4.4} = \underbrace{63.0 \text{ m}^2}_{22.5} = 22.5 \text{ m}^2 \\ A_4 = \underbrace{(12 + 2 \times 1.5)_{1.5}}_{2.8} = 49.2 \text{ m}^2 \\ A_5 = \underbrace{(12 + 2 \times 2.8)_{2.8}}_{2.7} = 46.9 \text{ m}^2 \end{aligned}$$

Trapozoidal 2

$$V = d \left[\frac{A_{1} + A_{0}}{2} + A_{2} + A_{3} + A_{4} \right]$$

= 100 $\left[\frac{36.08 + 46.9}{2} + 28.08 + 22.5 + 409.2 \right]$

= 14127 m3

prismoidal

3

$$= \frac{100}{3} \left[(36.08 + 46.9) + 4 (28.08 + 49.1) + 1(22.7) \right]$$

= 14587 m³ 14570

find out volume of earth work in a stoad cutting 120m long, from the center line as follows tosmation with 10m side slope lin 1 (n=1), Average depth of cutting along the centre line 5m, slope of ground in a c/s 10 to 1

8

$$A = \frac{\left[n \times \left(\frac{b}{2}\right)^{2} + m^{2} \left(bh + nh^{2}\right)\right]}{\left(m^{2} - n^{2}\right)}$$

b=10m 1to1 = n=/ h=3m 10to1=m=10

 $A = \left[\frac{\left(n \times \left(\frac{h}{2}\right)^{2} + m^{2} \left(\frac{b + nh^{2}}{2}\right)\right]}{m^{2} - n^{2}} \right]$ $= \left(1 \times \left(\frac{10}{2}\right)^{2} + 10 \left(10 \times 5 + 1 \times 5^{2}\right)\right)$ 10-1 = 76.01 m V = Axv V=76×120 = girong The following three level cross section of two stations of two stations som appart the width of tormation level 12m calculate volume of Cutting between two stations Station CIOSS Sections Alin 2.8, 4.6, 0.8 50m 1 2 2.9/8.9 3.7/0 69/12.9 Three level Statin D $A = \left[\frac{b}{y}(h_1 + h_2) + \frac{h}{2}(w_1 + w_2)\right]$ $= \left(\frac{12}{4} (u.6417) + \frac{2.8}{2} (10.6417)\right)$ b= 12m h = 2.8. A1= 44.52 mL W, 5 10.6 W2 = 7.7 $h_{1} = 46$ h2=1.7

D

Section ()

 $h = 3.7, \quad h_{1} = 6.9 \quad h_{2} = 2.9, \quad \omega_{1} = 1^{2}.9, \quad \omega_{1} = 8.9, \quad b = 1209$ $A_{\frac{1}{2}} \left[\frac{b}{4} (h_{1} + h_{2}) + \frac{h}{2} (\omega_{1} + \omega_{2}) \right]$ $= \left[\frac{12}{4} (6.9 + 2.9) + \frac{3.7}{2} (12.9 + 8.9) \right]$ $A_{2} = 69.73 \text{ m}^{2}$ Trape 30 id al $V = \left(\frac{A_{1} + A_{1}9}{2} \right) d$

$$= \left[\frac{44.52 \pm 69.13}{2} \right] 50$$

2 2856m³

parsmodial formula when in even case

$$V = \frac{L}{6} \left(A_1 + 4 \operatorname{Am} + A_2 \right)$$

psilsmoidal formula Three level = $\begin{pmatrix} b \\ 4 \end{pmatrix} (h_1 + h_1) + \frac{h}{2} (w_1 + w_2) \end{pmatrix}$ Even case $V = \frac{V}{6} A_1 + 4Am + A_2$ $Am = \frac{2}{5}$ b = 12m $h = 2.8 \rightarrow section @$ $h = \frac{2813.7}{2} = 3.25m$ $h = 3.7 \rightarrow section @$ $h_1 = 4.6 @ section @$ $h_1 = \frac{4.646.9}{2} = 5.75$ $h_1 = 6.9 @ section @$

$$w_{1} = 10.6 \ @ section 0 \qquad w_{1} = \frac{10.6 + 12.9}{2} = 11.75$$

$$w_{1} = 12.9 \ @ section 0 \qquad h_{12} = \frac{1.142.9}{2} = 2.3$$

$$h_{2} = 2.8 \ @ section 0 = 11 \qquad w_{2} = \frac{1.148.9}{2} = 8.3$$

$$w_{2} = 8.9 \ @ section 0 = 11 \qquad w_{2} = \frac{1.148.9}{2} = 8.3$$

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$$M_{2} = 8.9 \ @ section 0 = 11 \qquad w_{2} = \frac{1.148.9}{2} = 8.3$$

$$M_{2} = \frac{1}{4} \ (himmon + himmon) + \frac{himmon}{2} \ (w, mean + w_{2}, mean)$$

$$= \left[\frac{1}{4} (4.144.4 + A_{1}) + \frac{1}{2} = 8.3$$

$$M_{2} = \frac{50}{6} \ (A_{4.524} + 69.134 + 4.56.1) \right]$$

$$= \frac{50}{6} \ (A_{4.524} + 69.134 + 4.56.1) \right]$$

$$= \frac{50}{6} \ (A_{4.524} + 69.134 + 4.56.1) \right]$$

$$= \frac{50}{6} \ (A_{4.524} + 69.134 + 4.56.1) \right]$$

$$= \frac{50}{224.43n}$$

$$Volume of Baxrow pits (total area is divide 1 integes of Baxrow pits (total area is divide 1 integes 0 f Baxrow pits (total area is divide 1 integes 0 f Baxrow pits (total area is divide 1 integes 0 f Baxrow pits (total area is divide 1 integes 0 f Baxrow pits (total area is divide 1 integes 0 f Baxrow pits (total area is divide 1 integes 0 f Baxrow pits (total area is divide 1 integes 0 f Baxrow pits (total area is divide 1 integes 0 f Baxrow pits (total area is divide 1 integes 0 f Baxrow pits (total area is divide 1 integes 0 f Baxrow pits (total area is divide 1 integes 0 f Baxrow pits (total area is divide 1 integes 0 f Baxrow pits (total area is divide 1 integes 0 f Baxrow pits (total area is divide 1 integes 0 f Baxrow pits (total area is divide 1 integes 0 f Baxrow pits (total area is divide 1 intege$$

DJOPpeur

O A Rectangulasi plot ABCD forms a pit Excavated los Road work. E is a point of intersection of diagonals. Calculate volume of excavation at following points, length of AB som length of BC 80m. onin t

point	A	ß	C	a	E	P
ostiginal level	45,2	49.8	51.2	47.2	52.0	
final level	38.6	39.8	42.6	40.8	425	A 80m -

Solution:-

Repth of cutting at A = 45.2-BB,6 = 6.6m Depth of cutting at B = 49.8-39.8 = 10m Depth of certaing at c = 512-42.6 = 8.6m Repth of ceeting at D = 47.2 - 40.8 = 6.8m Repth of certaing at E= 52.0 - 42.5 = 9.5 m

Consider
$$ABE = \frac{hathbth}{3} = \frac{6.641049.5}{3} = 8.7m$$

 $A = \frac{1}{2} \times 50 \times 40 = 1000 \text{ m}^2 = 8.1 = (Areg. height) \times Area$

$$= \frac{1}{2} \times bxh$$

= $\frac{1}{2} \times 50 \times u0 = 1000 \text{ m}^2$
V = 8-7×1000 = 8700 m³

(a)
$$P = \frac{6.649.546.84}{3} = 7.63 = 1000 \times 7.63 = 7600 m^3$$

(b) $P = \frac{1049.548.6}{3} = 9.36 = 1000 \times 9.36 = 93.66 m^3$

An excavation to be made for a resorvery 20m long 12 m width at a bottom sustace have Side slope 2 in 1 calculate volume of excavation if Repth is 4m. The Ground surface is levelled before the excavation. Bm length of resolver at Top = Ltenh. 28 8 20 = 20+212xu = 36mB - 20m width of reservior at pop B'k = btznb length of reseavoir at mid height. $=\frac{20+36}{2}=28 m$ width of reservoirs at mid height 86 $=\frac{12+28}{2}=2000$ Side width = (28-20) = 8m Area of bottom Resouver = 20x12 = 240m Area at Top $= 36x2B = 1008m^2$ Area of resource out mid height = 28x20 = 560m² The area of ABCD And A'B'c'o' are parallel to each other since prismoidal formula can be used prismoidal formula at Gren $V = \frac{1}{6} \left(\frac{depth}{A_1 + A_2 + 4A_m} \right)$ = 4 (240+1008+560) = 2325 m3/

0

Cinil: 4

past A 1000 pasti- B Cleares Construction Survey -> rypes of carmey -> Introduction (setting out) > neccesty of cashes -> swilding setting out -) clements of sample cure -> culvert setting out -> setting out of cause Types of conver: (i) Havisontal, vertical curves Hoaizontal Curre ? (1) Simple curre (i) compound curre (1) Revease Curve Vertical curve i (i) summit () velly Simple Cashe: It consists of a single arc Compound Cuave: It consists of two (or) more single / asic's Reverse cusive :it consists of low Circular arcs with opposite direction Necessity of cuare: it is used to change the direction It is used to change the allignment It is used to cross obstrates 51 decreases spect

Elements b1 cuint; YN 1. Back Tangert - the distance from A to T. l'avoard Tangent - the distance from t_ - 0 3 point of cause (pc) - starting point cause is large as point of come 4 point of Intergrection (PJ) 5. point of tangency (21) - anding point of point odaw 6 Intersection angle - The angle blue vond vo 7 Deflection angle - the angle at any point on a came bloops and Pa 8 rangart distance () - distance blue pe de PS/PS topi T = Plan D 9 External distance (E) - distance from mid point of curre to pe to congth of cauve its - total length of crowe from Pe C. R×Sec D I reagth of chord to pr - the arc joints pe-pj L' = QR SIN = D long chosed - The oscillate from and point of long 1 R chose to mid point of custo Mid IS MINE ordinate (M) = $R\left(1 - \frac{(\cos \beta)}{2}\right)$

pasit :- B construction survey [setting outs] Introduction: It is a process of transferring the distance -Isroom the plan already prepased to the ground before setting is called Construction (a) Setting out the plan as designed and prepared is set out on the ground in the correct position Setting for the controls 1 Hoursontal controls buildings, have 2 restical control hages, but Setting out of building. It is depend on four edulion Instruct stel have two metallic lapse Right angle, source hommon 14.21 Ciacums cribing Rectangle - 21 -1- 11.11m SU TA ----- 10. Bm Porr Purm 0000 Priot 5m / Jh 50130 6.4 Vesor dan lourson



Curves: Definition and Types | Curves | Surveying

Definition of Curves:

Curves are regular bends provided in the lines of communication like roads, railways etc. and also in canals to bring about the gradual change of direction. They are also used in the vertical plane at all changes of grade to avoid the abrupt change of grade at the apex.

Curves provided in the horizontal plane to have the gradual change in direction are known as Horizontal curves, whereas those provided in the vertical plane to obtain the gradual change in grade are known as vertical curves. Curves are laid out on the ground along the centre line of the work. They may be circular or parabolic.

Classification of Curves:

(i) Simple,

- (ii) Compound
- (iii) Reverse and
- (iv) Deviation

(i) Simple Curve:

A simple curve consists of a single arc of a circle connecting two straights. It has radius of the same magnitude throughout. In fig. 11.1 T1 D T2 is the simple curve



with T1O as its radius.

(ii) Compound Curve:

A compound curve consists of two or more simple curves having different radii bending in the same direction and lying on the same side of the common tangent. Their centres lie on the same side of the curve. In fig. 11.2, T1 P T2 is the compound curve with T1O1 and PO2 as its radii.



(iii) Reverse (or Serpentine) Curve:

A reverse or serpentine curve is made up of two arcs having equal or different radii bending in opposite directions with a common tangent at their junction. Their centres lie of opposite sides of the curve. In fig. 11.3 T1 P T2 is the reverse curve with T1O1 and PO2 as its radii.



Reverse curves are used when the straights arc parallel or intersect at a very small angle. They are commonly used in railway sidings and sometimes on railway tracks and roads meant for low speeds. They should be avoided as far as possible on main railway lines and highways where speeds are necessarily high.

(iv) Deviation Curve:

A deviation curve is simply a combination of two reverse curves. It is used when it becomes necessary to deviate from a given straight path in order to avoid

intervening obstructions such as a bend of river, a building, etc. In fig. 11.4. T_1 EDFT₂ is the deviation curve with T_1O , EO₂ and FO₂ as its radii.



Names of Various Parts of a Curve: (Fig. 11.5):

(i) The two straight lines AB and BC, which are connected by the curve are called the tangents or straights to the curve.

(ii) The points of intersection of the two straights (B) is called the intersection point or the vertex.

(iii) When the curve deflects to the right side of the progress of survey as in fig. 11.5, it is termed as right-handed curve and when to the left, it is termed as left-handed curve.

(iv) The lines AB and BC are tangents to the curves. AB is called the first tangent or the rear tangent BC is called the second tangent or the forward tangent.

(v) The points (T_1 and T_2) at which the curve touches the tangents are called the tangent points. The beginning of the curve (T_1) is called the tangent curve point and the end of the curve (T2) is called the curve tangent point.

(vi) The angle between the tangent lines AB and BC (ABC) is called the angle of intersection (I) $% \left(1-\frac{1}{2}\right) =0$



(vii) The angle by which the forward tangent deflects from the rear tangent is called the deflection angle (ϕ) of the curve.

(viii) The distance the two tangent point of intersection to the tangent point is called the tangent length (BT_1 and BT_2).

(ix) The line joining the two tangent points (T_1 and T_2) is known as the long-chord

(x) The arc T_1FT_2 is called the length of the curve.

(xi) The mid-point (F) of the arc (T_1FT_2) in called summit or apex of the curve.

(xii) The distance from the point of intersection to the apex of the curve BF is called the apex distance.

(xiii) The distance between the apex of the curve and the midpoint of the long chord (EF) is called the versed sine of the curve.

(xiv) The angle subtended at the centre of the curve by the arc T_1FT_2 is known as the Central angle and is equal to the deflection angle (ϕ).

Elements of a Curve (Fig. 11.5):

(i) Angle of intersection + Deflection angle = 180° $I + \phi = 180^{\circ}$ or(Eqn. 11.1) -... (*ii*) $\angle T_1 O T_2 = 180^\circ - I = \phi$...(Eqn. 11.2.) (*i.e.* the central angle = the deflection angle). (*iii*) Tangent length = BT₁ = BT₂ = OT₁ tan $\frac{\varphi}{2}$ $= R \tan \frac{\phi}{2} \qquad \dots \qquad \dots$...(Eqn. 11.3) (*iv*) Length of Long Chord = $2T_1E = 2 \times OT_1 \sin(\frac{\phi}{2})$ $= 2R \sin \frac{\Phi}{2}$ (Eqn. 11.4) (v) Length of the curve = Length of the arc T_1FT_2 = $R\phi$ (in radians) $= \frac{\pi R\phi}{180^{\circ}}$ (vi) Apex distance = BF = BO - OF (Eqn. 11.5) $= R \sec \frac{\Phi}{2} - R$ = $R\left(\sec(\frac{\phi}{2}-1) \dots \dots (Eqn. 11.6)\right)$ (vii) Versed sine of the curve = EF = OF – $= R - R \cos \frac{\Phi}{2}$ = $R\left(1 = \cos\frac{\phi}{2}\right) = R$ versine $\frac{\phi}{2}$ (Eqn. 11.7)

Designation of Curves:

A curve may be designated either by the radius or by the angle subtended at the centre by a chord of particular length In India, a curve is designated by the angle (in degrees) subtended at the centre by a chord of 30 metres (100 ft.) length. This angle is called the degree of the curve (D).

The relation between the radius and the degree of the curve may be determined as follows:

Refer to fig 11.6:



Let R= The radius of the curves in meters

D= The degree of the curve

MN= The chord, 30m long

P= The mid-point of the chord

In
$$\triangle$$
 OMP, OM = R

$$MP = \frac{1}{2}MN = 15 m$$

$$\angle MOP = \frac{D}{2}$$
Then, $\sin \frac{D}{2} \equiv \frac{MP}{OM}, \frac{15}{R}$
or
$$R = \frac{15}{\sin \frac{D}{2}} \quad (Exact) \quad \dots \quad ... (Eqn. 11.8)$$

But when D is small, sin $\frac{D}{2}$ may be assumed approximately equal to

 $=\frac{D}{2}$ in radians.

$$R = \frac{15}{\frac{D}{2} \times \frac{\pi}{180^{\circ}}} = \frac{15 \times 360}{\pi D}$$
$$= \frac{171.87}{D}$$
or say, R = $\frac{1719}{D}$ (approximate) (Eqn. 11.9)

The approximate relation holds good up to 5° curves. For higher degree curves, the exact relation should be used.

Methods of Curve Ranging:

A curve may be set out:

1. By linear methods, where chain and tape are used.

2. By angular or instrumental methods, where a theodolite with or without a chain is used.

Before starting setting out a curve by any method, the exact positions of the tangent points between which the curve lies, must be determined.

For this, proceed as follows: (Fig. 11.5)

(i) Having fixed the directions of the straights, produce them to meet at point (B).

(ii) Set up a theodolite at the intersection point (B) and measure the angle of intersection (I). Then find the deflection angle (ϕ) by subtracting (I) from 180° . i.e., $\phi = 180^{\circ}$ — I

(iii) Calculate the tangent length from the Eqn. 11.3:

$$\left(\tan \text{lenght} = \text{R} \tan \frac{\Phi}{2} \right)$$

(iv) Measure the tangent length (BT_1) backward along the rear tangent BA from the intersection point B, thus locating the position of T_1 .

(v) Similarly, locate the position of T_2 by measuring the same distance forward along the forward tangent BC from B,

Having located the positions of the tangent points T_1 and T_2 ; their changes may be determined. The change of T_1 is obtained by subtracting the tangent length from the known change of the intersection point B. And the change of T_2 is found by adding the length of the curve to the change to T_1 .

Then the pegs are fixed at equal intervals on the curve. The interval between the pegs is usually 30 m or one chain length. This distance should actually be measured

along the arc, but in practice it is measured along the chord, as the difference between the chord and the corresponding arc is small and hence negligible. In order that this difference is always small and negligible, the length of the chord should not be more than 1/20th of the radius of the curve. The curve is then obtained by joining all these pegs.

The distances along the centre line of the curve are continuously measured from the point of beginning of the line up to the end, i.e., the pegs along the centre line of the work should be at equal interval from the beginning of the line to the end. There should be no break in the regularity of their spacing in passing from a tangent to a curve or from a curve to a tangent.

For this reason, the first peg on the curve is fixed at such a distance from the first tangent point (T_1) that its change becomes the whole number of chains i.e. the whole number of peg interval. The length of the first chord is thus less than the peg interval and is called as a sub- chord. Similarly, there will be a sub chord at the end of the curve. Thus, a curve usually consists of two-chords and a number of full chords. This is made clear from the following example.

Linear Methods of Setting out Curves

The following are the methods of setting out simple circular curves by linear methods and by the use of chain and tape: 1. By ordinates from the Long chord 2. By Successive Bisection of Arcs. 3. By Offsets from the Tangents. 4. By Offsets from Chords Produced.

Method # 1. By Ordinates from the Long Chord (Fig. 11.8):

Let T1T2=L= the length of the Long chord

ED= O0= the offset at mid-point (e) of the long chord (the versed sine)

PQ=Ox= the offset at distance x from E

Draw QQ1 parallel to T1 T2 meeting DE at Q1



When the radius of the curve is large as compared with the length of the long chord, the offset may be equated by the approximate formula which is derived as follows:

Here Ox is assumed to be equal to the radial ordinate QP1.

$$QP \times 2R = T_1P \times PT_2$$

 $QP_1 = \frac{T_1 P \times P T_2}{2P}$ or Now $T_1P = x$, and $PT_2 = L - x$

 $Q_x = \frac{x(L-x)}{2R}$ (approximate)(Eqn. 11.11)
Note:

In the exact equation (11.1), the distance x of the point P is measured from the mid-point of the long chords; while in the approximate equation (11.11), it is measured from the first tangent point (T1).

Procedure of Setting Out the Curve:

(i) Divide the long chord into an even number of equal parts.

(ii) Calculate the offsets by the equation 11.10 at each of the points of division.

Note:

1. Since the curve is symmetrical on both sides of the middle- ordinate, the offsets for the right-hand half of the curve are the same as those for the left-hand half.

ADVERTISEMENTS:

2. If the offsets are found by the approximate equation (11.11), the long chord should be divided into a convenient number of equal parts and the calculated offsets laid out at each of the points of division.

This method is used for setting out short curves e.g., curves for street bends.

Method # 2. By Successive Bisections of Arcs (Fig 11.10):

It is also known as Versine Method. Join T1 T2 and bisect it at E. Set out the offset ED the versed since equal to:





Join T1D and DT2 and bisect them at F and G respectively. Then set outsets FH and GK at F and G each equal to $R\left(1-\cos\frac{\Phi}{4}\right)$ thus fixing two more points H and K on the curve. Then each of the offsets to be set out at mid points of the chords T1H, HD, DK and KT2 is equal to $R\left(1-\cos\frac{\Phi}{8}\right)$.By repeating this process, set out as many point as are required.

This method is suitable where the ground outside the curve is not favorable to the tangents.

Method # 3. By Offsets from the Tangents:

The offsets may be either radial or perpendicular to the tangents.

(a) By Radial Offsets (Fig 11.11a):



Let $O_x = PP_1$ = the radial offset at P at a distance of x from T₁ along the tangent AB

$$PP_1 = OP - OP_1$$
, where $OP = \sqrt{R^2 + x^2}$ and $OP_1 = R$
 $O_x = \sqrt{R^2 + x^2} - R$ (exact)(Eqn. 11.12)

When the radius is large, the offsets may be calculated by the approximate formula, which may be derived as under:

$$PT_1^2 = PP_1 \times (2R + PP_1)$$

i.e. $x^2 = O_x (2R + O_x) = 2RO_x + O_x^2$
Since O_x^2 is very small as compared with 2R, it may be neglected.
 $x^2 = 2R.O_x$
or $O_x = \frac{x^2}{2R}$ (approximate)(Eqn. 11.13)

(b) By Offsets perpendicular to the Tangents (Fig 11.11,b):

Let $O_x = PP_1$ = the perpendicular offset at P at a distance of x from T_1 along the tangent AB.

Draw P₁P₂ parallel to BT₁, meeting OT₁ at P₂ Then P₁P₂ = PT₁ = x; T₁P₂ = PP₁ = O_x. Now T₁P₂ = OT₁ — OP₂ where OT₁ = R, and OP₂ = $\sqrt{R^2 - x^2}$ $O_x = R - \sqrt{R^2 - x^2}$ (exact)(Eqn. 11.14)



The approximate formula may be obtained similarly as in (a) above,

$$O_x = \frac{x^2}{2R} \qquad (approximate) \qquad \dots (Eqn. 11.15)$$

Procedure of setting out the curve:

(i) Locate the tangent points T1 and T2.

(ii) Measure equal distances, say 15 or 30 m along the tangent from T1.

(iii) Set out the offsets calculated by any of the above methods at each distance, thus obtaining the required points on the curve.

(iv) Continue the process until the apex of the curve is reached.

(v) Set out the other half of the curve from the second tangent.

This method is suitable for setting out sharp curves where the ground outside the curve is favourable for chaining.



Method # 4. By Offsets from Chords Produced (Fig. 11.12):

Let AB = the first tangent; T1 = the first tangent point E, F, G etc. on the successive points on the curve T1E = T1E1 = C1 = the first chords.

EF, FG, etc. = the successive chords of length C2, C3 etc., each being equal to the full chord.

 \angle BT1E = α in radians = the angle between the tangents BT1 and the first chord T1E.

E1E = O1 = the offset from the tangent BT1

E2F = O2 = the offset from the chord T1E produced.

Produce T1E to E2 such tharEE2 = C2. Draw the tangent DEF1 at E meeting the first tangent at D and E2F at F1.

 \angle BT1E= α in the radians= the angle between the tangents BT1and the first chord T1E.

E1E=O1= the offset from the tangent BT1

E2F=O2= the offset from the chord T1E produced.

Produce T1E to E2 such that EE2= C2. Draw the tangent DEF1at E meeting the first tangent at D and E2Fat F1.

The formula for the offsets may be derived a under:

∠ BT1E=x

∠T1OE=2x

The angle subtended by any chord at the center is twice the angle between the chord and the tangent

$$\frac{\operatorname{arc} T_1 E}{\operatorname{Radius} OT_1} = 2\alpha$$

But arc T_1E is approximately equal to chord $T_1E = C_1$

$$\frac{C_1}{R} = 2\alpha$$

or

 $\alpha = \frac{C_1}{2R}$

Also

$$\frac{\operatorname{arc} E_{1}E}{T_{1}E} = \alpha$$

But arc E_1E is approximately equal to chord $E_1E = O_1$

$$O_1 = C_1 \times \alpha$$

Putting here the value of α as calculated above.

$$O_1 = C_1 \times \frac{C_1}{2R} = \frac{C_1^2}{2R}$$
 (Eqn. 11.16)

$$O_2 = offset E_2F = E_2F_1 + F_1F$$

To find out F2F1, consider the two triangles T1EE1 and EF1E2

 $\angle E_2 EF_1 = \angle DET_1$ (vertically opposite angles) :

 $\angle DET_1 = \angle DT_1E$, since $DT_1 = DE$, both being trangents to the circle.

$\angle E_1 EF_1 = \angle DET_1 = \angle DT_1 E$

Both the Δs being nearly isosceles, may be taken as approximately similar.

$$\frac{E_2F_1}{EE_2} = \frac{E_1E}{T_1E_1}$$

i.e.
$$\frac{\alpha}{E_2F_1} = \frac{O_1}{C_1}$$

=

or

$$E_2F_1 = \frac{C_2 \times O_1}{C_2}$$

$$\frac{C_2}{C_1} \times \frac{C_1^2}{2R} = \frac{C_1 C_2}{2R}$$

F1F being the offset from the tangent at E, is equal to

$$\frac{\mathrm{EF}^2}{2\mathrm{R}} \equiv \frac{\mathrm{C}_2^2}{2\mathrm{R}}$$

the second offset,
$$O_2 = \frac{C_1C_2}{2R} + \frac{C_2^2}{2R}$$

 $=\frac{C_2(C_1+C_2)}{2R}$... (Eqn. 11.17)

Similarly the third offset, $O_3 = \frac{C_3(C_2 + C_3)}{2R}$

Since

the
$$C_2 = C_3 = C_1$$
.....etc,
 $O_3 = \frac{C_2^2}{R}$ (Eqn. 11.18)

Each of the remaining offsets O4,O5 etc expect the last one (On) is equal to O3. Since the length of the last chord is usually less than the length of the chord, the last offset,

$$O_n = \frac{C_n (C_{n-1}+C_n)}{2R}$$
 = ... (Eqn. 11.19)

Procedure of Setting out the Curve (Fig. 11.12):

(i) Locate the tangent points (T1 and T2) and find out their changes. From these changes, calculate lengths of first and last sub-chords and find out the offsets by using the equations 11.16 to 11.19.

(ii) Mark a point E1 along the first tangent T1B such that T1E1 equals the length of the first sub-chord.

(iii) With the zero end of the chain (or tape) at T1 and radius = T1E1, swing an arc E1E and cut off E1E = O1, thus fixing the first point E on the curve.

(iv) Pull the chain forward in the direction of T1E produced until the length EE2 becomes equal to the second chord C2.

(v) Hold the zero end of the chain at E. and radius = C2, swing an arc E2F and cut off E2F = O2, thus fixing the second point F on the curve.

(vi) Continue the process until the end of the curve is reached. The last point fixed in this way should coincide with the previously located point T2. If not, find the closing error. If it is large i.e., more than 2 m, the whole curve are moved sideways by an amount proportional to the square of their distances from the tangent point T1. The closing error is thus distributed among all the points.

This method is very commonly used for setting out road curves.

Angular Methods for Setting out Curves

The following two methods are the methods of setting out simple circular curves by angular or instrumental methods: 1. By Rankine's Tangential Angles. 2. By Two Theodolites.

Method # 1. Rankine's Method of Tangential or Deflection Angles: (Fig. 11.14):

In this method, the curve is set out by the tangential angles (also known as deflection angles) with a theodolite and a chain (or tape). The method is also called as chain and theodolite method.

The deflection angles are calculated as follows:



Let T1 and T2 be the tangent points and AB the first tangent to the curve.

D, E, F, etc. =the successive points on the curve,

R = the radius of the curve.

C1, C2, C3 etc. = the lengths of the chords T1D, DE, EF etc., i.e., 1st, 2nd, 3rd chords etc.

ADVERTISEMENTS:

 δ 1, δ 2, δ 3 etc. = the tangential angles which each of the chords T1 D1, DE, EF, etc., makes with the respective tangents T1, D, E. etc.

 \triangle 1, \triangle 2, \triangle 3 etc. = the total tangential or deflection angles which the chords T1D, DE, EF, etc. make with the first tangent AB.

Since each of the chord lengths C2, C3, C4..... Cn-1 is equal to the length of the full chord, $\delta 2 = \delta 3 = \delta 4$ δ n-1.

The total tangential angle (Δ_1) for the first chord (T_1D) = $\angle BT_1D = \delta_1$ $\therefore \qquad \Delta_1 = \delta_1$ The total tangential angle (Δ_2) for the second chord (DE) = $\angle BT_1E$ But $\angle BT_1E = \angle BT_1D + \angle DT_1E$

It is well known preposition of geometry that the angle between the tangent and a chord equals the angle which the chord subtends in the opposite segment.

Now \angle DT1E is the angle subtended by the chord DE in the opposite segment, therefore, it is equal to the tangential angle (δ 2) between the tangent D and the chard DE

$$\begin{array}{ll} \therefore & \Delta_2 = \delta_1 + \delta_2 = \Delta_1 + \delta_2 \\ \text{Similarly,} & \Delta_3 = \delta_1 + \delta_2 + \delta_3 = \Delta_2 + \delta_3 \\ \therefore & \Delta_n + \delta_1 + \delta_2 + \delta_3 \dots + \delta_n \\ & = \Delta_{n-1} + \delta_n & \dots & \dots \text{(Eqn. 11.22)} \end{array}$$

Check:

The total deflection angle BT1 T2

$$=\Delta n = \frac{\Phi}{2}$$

where ϕ is the deflection angle of the curve.

If the degree of die curve (D) is known, the deflection angle for 30 m chord is equal 1/2D degrees, and that for the sub-chord of length C1,

$$= \frac{C_1}{30} \times \frac{D}{2} \text{ degrees}$$

$$\delta_1 = \frac{C_1 \times D}{60} ; \quad \delta_2 = \delta_3 \dots \delta_{n-1} = \frac{D}{2} ;$$

$$\delta_n = \frac{C_n \times D}{60} \dots \dots \dots \dots \dots \dots \dots \dots (\text{Eqn. 11.23})$$

Procedure of Setting out the Curve:

(i) Locate the tangent points (T1 and T2) and find out their changes. From these changes, calculate the lengths of first and last sub-chords and the total deflection angles for all points on the curve as described above.

(ii) Set up and level the theodolite at the first tangent point (T1).

(iii) Set the Vernier A of the horizontal circle to zero and direct the telescope to the ranging rod at the intersection point B and bisect it.

(iv) Loosen the Vernier plate and set the Vernier A to the first deflection angle $\Delta 1$, the telescope is thus directed along T1D. Then along this line, measure T1D equal in length to the first sub-chord, thus fixing the first point D on the curve.

(v) Loosen the upper clamp and set the Vernier A to the second deflection angle $\triangle 2$, the line of sight is now directed along T1E. Hold the zero end of the chain at D and swing the other end until the arrow held at that end is bisected by the line of sight, thus fixing the second point (E) on the curve.

(vi) Continue the process until the end of the curve is reached. The end point thus located must coincide with the previously located point (T2). If not, the distance between them is the closing error. If it is within the permissible limit, only the last few pegs may be adjusted; otherwise the curve should be set out again.

Note:

In the case of a left-handed curve, each of the values $\Delta 1$, $\Delta 2 \Delta 3$ etc, should be subtracted from 360° to obtain the required value to which the vernier is to be set i.e. the vernier should be set to (360° - $\Delta 1$), (360° - $\Delta 2$), (360° - $\Delta 2$) etc. to obtain the 1st, 2n, 3rd etc, points on the curve.

This method gives highly accurate results and is most commonly used for railway and other important curves.

Point	Chainage in metres	Length of chord in metres	Deflection Angle (δ)	Total Angle (Δ)	Theodolite vernier Reading	Remarks
TL	39 + 6.30	a i #	0.4	o · *		
1	4() + 00	23.70	1 58 30	1 58 30	1 58 40	The curve is a
2	41 + 00	30	2 30 00	4 28 30	4 28 40	right-handed
3	42 + 00	30	2 30 00	6 58 30	6 58 40	one.
4	43 + 00	30	2 30 00	9 28 30	9 28 40	The least
5	44 + 00	30	2 30 00	11 58 30	11 58 40	count of the
6	45 + 00	30	2 30 00	14 28 30	14 28 40	instrument in
7	46 + 00	30	2 30 00	16 58 40	16 58 40	20 "
T2	46 + 12.30	12.30	1 01 30	18 00 00	18 00 00	

Table of Deflection Angles

Method # 2. Two-Theodolite Method (Fig. 11.16):

This method is very useful in the absence of chain or tape and also when ground is not favorable for accurate chaining. This is simple and accurate method but requires essentially two instruments and two surveyors to operate upon them, so it is not as commonly used as the method of deflection angles. In this method, the property of circle 'that the angle between the tangent and the chord equals the angle which that chord subtends in the opposite segment' is used.



Let D, E, F, etc. be the points on the curve. The angle (Δ 1) between the tangent T1B and the chord T1D i.e. \angle BT1 D = \angle T1T2D. Similarly, \angle BT1E = Δ 2 = \angle T1T2 E, and \angle BT1F = Δ 3 = \angle T1T2F etc. The total deflection angles Δ 1, Δ 2, Δ 3, etc. are calculated from the given data as in the first method (i.e. as in Rankine's method of deflection angles).

Procedure of setting out the curve:

(i) Set up two theodolites, one at T1 and the other at T2.

(ii) Set Vernier of the horizontal circle of each of the theodolites to zero.

(iii) Turn the instrument at T1 to sight the intersection point B and that at T2 to sight T1.

(iv) Set the Vernier of each of the instruments to read the first deflection angle $\Delta 1$. Now the line of sight of the instrument at T1 is along T1D and that of the instrument at T2 is along T2D. Their point of intersection is the required point on the curve Direct the assistant to move the ranging rod until it is sighted exactly by both the theodolites, thus fixing the point D on the curve.

(v) Then set the Vernier of each of the instrument to the second deflection angle $\Delta 2$, proceed as before to obtained the second point (E) on the curve.

(vi) Repeat the process until the whole curve is set out.

Note:

It may so happen that the point T1 may not be visible from the point T2. In such a case, direct the telescope of the instrument at T2 towards B with the Vernier A set to zero. Now loosen the Vernier plate and set the Vernier A to read an angle of $(360 \circ - \frac{\Phi}{2})$. The telescope is thus directed along T2 T1. For the first point D on the curve, set the Vernier A to read $(360 \circ - \frac{\Phi}{2} + \Delta_1)$. Similarly, for the second point E, set the Vernier A to $(360 \circ - \frac{\Phi}{2} + \Delta_2)$, and so on.

Transition Curves:

A non-circular curve of varying radius introduced between a straight and a circular curve for the purpose of giving easy changes of direction of a route is called a transition or easement curve. It is also inserted between two branches of a compound or reverse curve.

Advantages of providing a transition curve at each end of a circular curve:

(i) The transition from the tangent to the circular curve and from the circular curve to the tangent is made gradual.

(ii) It provides satisfactory means of obtaining a gradual increase of super-elevation from zero on the tangent to the required full amount on the main circular curve.

(iii) Danger of derailment, side skidding or overturning of vehicles is eliminated.

(iv) Discomfort to passengers is eliminated.

Conditions to be fulfilled by the transition curve:

(i) It should meet the tangent line as well as the circular curve tangentially.

(ii) The rate of increase of curvature along the transition curve should be the same as that of increase of super-elevation.

(iii) The length of the transition curve should be such that the full super-elevation is attained at the junction with the circular curve.

(iv) Its radius at the junction with the circular curve should be equal to that of circular curve.

There are three types of transition curves in common use:

(1) A cubic parabola,

(2) A cubical spiral, and

(3) A lemniscate, the first two are used on railways and highways both, while the third on highways only.

When the transition curves are introduced at each end of the main circular curve, the combination thus obtained is known as combined or Composite Curve.

Super-Elevation or Cant:

When a vehicle passes from a straight to a curve, it is acted upon by a centrifugal force in addition to its own weight, both acting through the centre of gravity of the vehicle. The centrifugal force acts horizontally and tends to push the vehicle off the track.

In order to counteract this effect the outer edge of the track is super elevated or raised above the inner one. This raising of the outer edge above the inner one is called super elevation or cant. The amount of super-elevation depends upon the speed of the vehicle and radius of the curve.





Let:

W = the weight of vehicle acting vertically downwards.

F = the centrifugal force acting horizontally,

- v = the speed of the vehicle in meters/sec.
- g = the acceleration due to gravity, 9.81 meters/sec².
- R = the radius of the curve in meters,
- h = the super-elevation in meters.

 ${\sf b}$ = the breadth of the road or the distance between the centres of the rails in meters.

Then for equilibrium, the resultant of the weight and the centrifugal force should be equal and opposite to the reaction perpendicular to the road or rail surface.

The centrifugal force	F =	Wv^2
The contrugation to co,		gR
	F	v^2
••	w≡	gR

If $\,\theta\,$ is the inclination of the road or rail surface, the inclination of the vertical is also $\,\theta\,$

$$\tan \theta = \frac{dc}{ac} = \frac{F}{W} = \frac{v^2}{gR}$$

uper-elevation = b tan θ .
$$= \frac{bv^2}{gR} \qquad \dots \qquad \dots \qquad (Eqn. 11.28)$$

Characteristics of a Transition Curve (Fig 11.25):

Here two straights AB and BC make a deflection angle Δ , and a circular curve EE' of radius R, with two transition curves TE and E'T' at the two ends, has been inserted between the straights.

(i) It is clear from the figure that in order to fit in the transition curves at the ends, a circular imaginary curve $(T_1F_1T_2)$ of slightly greater radius has to be shifted towards the centre as ($E_1 \ EF \ E \ E_1$. The distance through which the curve is shifted is known as L^2

shift (S) of the curve, and is equal to 24R, where L is the length of each transition curve and R is the radius of the desired circular curve (EFE'). The length of shift (T₁E₁) and the transition curve (TE) mutually bisect each other.

Fig. 11.25:



(ii) The tangent length for the combined curve

= OT₁ tan
$$\frac{\Delta}{2} + \frac{L}{2}$$

= (R + S) tan $\frac{\Delta}{2} + \frac{L}{2}$
(iii) The spiral angle $\phi_{1} = \frac{\frac{L}{2}}{R} = \frac{L}{2R}$ radians

(iv) The central angle for the circular curve:

$$\angle EOE' = \triangle 2 \varphi_1$$

(v) Length of the circular curve EFE'

$$= \frac{\pi R(\Delta - 2\phi_1)}{180^{\circ}}, \text{ where } \Delta \text{ and } \phi_1 \text{ are in degrees.}$$

(vi) Length of the combined curve TEE'T"



(vii) Change of beginning (T) of the combined curve = Change of the intersection point (B)-total tangent length for the combined curve (BT).

(viii) Change of the junction point (E) of the transition curve and the circular curve = Change of T + length of the transition curve (L).

(ix) Change of the other junction point (E') of the circular curve and the other transition curve-change of E + length of the circular curve.

(x) Change of the end point (T') of the combined curve = change of E' + length of the transition curve.

Check:

The change of T thus obtained should be = change of T + length of the combined curve.

Note:

The points on the combined curve should be pegged out with through change so that there will be sub-chords at each end of the transition curve and of the circular curve.

(xi) The deflection angle for any point on the transition curve distant I from the beginnings of combined curve (T),

$$\alpha = \frac{l^2}{6RL} \text{ radians} = \frac{1800l^2}{\pi RL} \text{ minutes.}$$
$$= \frac{573l^2}{RL} \text{ minutes.}$$

Check:

The deflection angle for the full length of the transition curve:

$$\alpha = \frac{l^2}{6RL} = \frac{L^2}{6RL} \quad (\because l = L)$$
$$= \frac{L}{6R} \text{ radians} = \frac{1}{3}\phi_1$$

(xii) The deflection angles for the circular curve are found from:

$$\delta_n = 1718.9 \frac{C_n}{R}$$
 minutes.

Check:

The deflection angle for the full length of the circular curve:

$$\Delta_n = \frac{1}{2} \times Central angle$$

i.e.,
$$\Delta_n = \frac{1}{2} \times (\Delta - 2\emptyset_1)$$

(xiii) The offsets for the transition curve are found from:

Perpendicular offset, $y = \frac{x^3}{6RL}$, where x is measured along the tangent TB

Tangentail offset , $y = \frac{l^3}{6RL}$, where I is measured along the curve

Check: (a) The offset at half the length of the transition curve,

$$y = \frac{l^3}{6RL} = \frac{(L/2)^3}{6RL} (\because l = L/2)$$
$$= \frac{L^2}{48R} = \frac{1}{2}S$$

(b) The offset at junction point on the transition curve,

$$y = \frac{l^3}{6RL} = \frac{L^3}{6RL} = \frac{L^2}{6R}(\because l = L)$$

= 4S

(xiv) The offsets for the circular curve from chords producers are found from:

$$O_n = \frac{C_n \left(C_{n=1} + C_n \right)}{2R}$$

an quantum e Sa

Method of Setting Out Combined Curve by reflection Angles (Fig. 11.25):

The first transition curve is set out from T by the deflection angles and the circular curve from the junction point E. The second transition curve is then set out from T' and the work is checked on the junction point E' which has been previously fixed from E.

(i) Assume or calculate the length of the transition curve.

(ii) Calculate the value of the shift by:

$$S = \frac{L^2}{24R}$$

(iii) Locate the tangent point T by measuring backward the total tangent length BT (article 11.14, ii) from the intersection point B along BA, and the other tangent T by measuring forward the same distance from B along BC.

(iv) Set up a theodolite at T, set the Vernier A to zero and bisect B.

(v) Release the upper clamp and set the Vernier to the first deflection angle (x_1) As obtained from the table of deflection angles, the line of sight is thus directed along the first point on the transition curve. Place zero end of the tape at T and measure

along this line a distance equal to first sub chords, thus locating first point on the transition curve.

(vi) Repeat the process, until the end of the curve E is reached.

Check:

The last deflection angle should be equal to $\phi_1/3$, and the perpendicular offset from the tangent TB for the last point E should be equal to 4S.

Note:

The distance to each of the successive points on the transition curve is measured from T.

(vii) Having laid the transition curve, shift the theodolite to E and set it up and level it accurately.

(viii) Set the Vernier to a reading($360^{\circ} -2/3 \ \phi \ 1$) for a right-hand curve (or $2/3 \ \phi \ 1$) for a left-hand curve and lake a back sight on T. Loosen the upper clamp and turn the telescope clockwise through an angle $2/3 \ \phi \ 1$ the telescope is thus directed towards common tangent at E and the Vernier reads 360° . Transit the telescope, now it points towards the forward direction of the common tangent at E i.e. towards the tangent for the circular curve.

(ix) Set the Vernier to the first tabulated deflection angle for the circular curve, and locate the first point on the circular curve as already explained in simple curves.

(x) Set out the complete circular curve up to E' in the usual way

Check:

The last deflection angle should be equal to $\frac{1}{2}(\Delta-2\varphi_1)$

(xi) Set out the other transition curve from T as before. The point E' to be set from T should be the same as already set out from E.

Method of Setting Out a Combined Curve by Tangential Offsets (Fig. 11.25):

(i) Assume or calculate the length of the transition curve.

(ii) find the value of the shift train, $S = \frac{L^2}{24R}$

(iii) Locate the tangent points T and T as in article (11.15, iii),

(iv) Calculate the offset for the transition curve as in article (11.14 xiv)

(v) Locate die points on the transition curve as well as on the circular curves by setting out the respective offsets.

UNIT -5

MODERN FIELD SURVEY SUSTEMS

EDM

- * Measurement principle of FOM
- * characteristics of EDM.
- * Accusacy in EDM.
- Total station
- * Introduction
- * Advantages and types
- * Applications
- * field procedure

DGES

- * Introduction
- * wosking psincipal
- * Daps receivers
- * Application
- * LIDAR

Methods of distance measurement

- 1. DDM er, Direct distance measurement:-This is mainly done by chaining (er, Taping.
- 2 ODM (or) optical distance measurement :-

This measurement is conducted by tacheometry borizontal subtense method by telemetric method. These are carried out with the help of optical wedge atlachments 3. EDM according electromagnetic Didance massurements What is EDMS

★ It is a surveying instrument and II is used for measursing distance electronically, between two p.
through the electromagnetic rays.
★ EDM has a accuracy of 1 In 10⁵, and distance is 100 Icm.
The wave's are used in EDM.
I. Micro wave - long range, trag 3-30 GH2, Tellissometer
9 Visible light - medium, trag 5×10¹⁴H2, Geodimeter
5. Intraved - short, trag 5×10¹⁴H2, Ristomat
Basic functions:Generation, modulation -> Tansmission -> propagation -> Reflections
Reception - Remodulation -> distance measurement

Applications of T.s

* Detailed survey

of controlled survey

* Height measurement

* Fixing of missing pillary

* Reseaction

+ Area calculations Gtc

+ Remote distance measurement le phylor, missing lie Measurement.

1st unit formulas Tompestature - 4= & (Im- to) L length = L' x measured distance pull = P-Po)co sag = LWL slope= h L(1-coso) 763 0 M weis - to weis was 270 00- 0- 00 NE WCB SE 180-WCD 180 8 W WC0-180 $BD = FO \pm 180$ NW 360-00CO

Included angle = B.B of pserious line - F-B of Acadli Check (2n-u) go Rease and frace method Iteight of Instaument In these method where the place is shift at that point is FS and that shifted front side is BS: Unit -5 mertion

Electronic Distance Measurement and

Remote Sensing

GITS A VI a GIT Greagraphic Information system

* It is an computer based, tool for mapping analysing thing's that exist and events and that happen's on earth.

Gis technology integrates common database × Operatation such as query & statictical analysis with Unique visualization and geographic analysis benifit's offered by analysis

principle's of Gils

hemes

* It containastores information about the world as a collection of thematic layer that Can be linked together by geography. and anothing the short

land use pattern

Road Network

Topography

water Distribution Network.

* Geographic references drainage system

Top f1007 at on the second floor investigat 1 First floor Ground floor Foundation floor wile information VL nultanutal urlgovard 2009 Studente) 21 13 2008 pende pendylara bas 2007 in impact with 200 b contaminat and s damente y fer de WORK ALLOW INVIOLO Time period. stilling titlions * It contain's Rither an explicit geographic reference, such as latitude and longitude (on National grid co-ordinate, (on an implicit reference such as address, postal code , cencus Name, forst Details etc. AND GARDENNE Gis system 197. C Raster 1.0 g St ... Vector Made 1 model . Scanned with CamScanner

Components of Gils hediant A working Gis Integrates five Key components light in any light in a 1. software Applications of Control 2. Hardware 3. Data 4. people 5. method in D landacid di 1. Software la langets l'anti manufe * Tool for input & manipulation of GIS A database Management system ¥ Maria Parala 2. Hardware * It's a computer on which Gils operates. 10. 10 3. Dota Most important contact & component of a Gils is the Data geographic data and related tabulated data (an be Collected in house or) purchased from a commercial data provider. 4. people. Gis technology is of limited value with Out the people who manage the system and Jevelop plans for applying it to real world problems.

Method A successful Gis operates according to a well Designed plan an Method.

Applications of GUS:0

* Inconcept OF Geographic information Infrastructure has brought about a dramatic philosophical and technological revolutions in the Development of GU * GLS is became an important tool for & GLS is became an important tool for Natural Resources.

Major Operation areas

1. Academic * Research in engineering | sciences * Humanities & Science.

2. Industry

* surveying f mapping

x Transportation - vehicle tracking

* forestry and Repurces.

3 Business

* Banking

* Real (state - Building management

Government * National topography mapping * voting * Surveying and mapping * waste water Service I management Military * Training, command of control * Intelligence gathering in shead Electronic Distance Measurement EDM Million all y Introduction * EDM's are mountable with optic/ electronic thodolites X EDM was first Introduced in 1950. * Inifially EDM used to Measure Distance * Electronic theodolite was rapid q advance technology they are available in lighter, simpler and less expansive instruments Now adays. Bach. N principles of EDM EDM. 用----M M



Where

C - velocity in Emlsec

A - wave length in metres

 $\gamma = \frac{t}{c}$

f - trequency in Hz (cyclelsec) !

* The principle of EDM comently used in Total Station. Distance Measurement through waves in

Types of EDM

Depending upon Different wave length

1. Infrared wave Instrument

2. light wave system

3. microware Instrument

4. Geodimeter

5. Jellurometer.

6. Distomat

Pullo 1

7. Electronic theodolite

AV V

(Sel)

Mad to

Infrored System / Instrument

* This equiprement helped & working with modulated infrared waves. * The use of Infrared Instrument is high in civil engineering survey work's. * although these type of Instruments used to measure maximum Distance of about 3 to 5 km only. * Distomates, electronic theodolites of total station comes under this category. * In this system, Instruments are having accuracy of ± lomm per km Can be

obtained.

Electronic theodolite's of Total Station

* Vernier theodolite have least count of 20" (or) 10".

* Micro optical electronic theodolite having least count of 0.1".

* Electronic theodolites are the most occurate Intrumenti For direct

observations.

* These Introments works withe electronic speed & Most accurasy. User of Electronic Theodolite.

* Used for angle Measurement * Used for Wide Distance for Angular and Distance Measurement * It is Compatable with theodolite Accessaries * It Can connect with Computer throw

RS 232 interface connection.

Total Station

Total station is a combination of electronic theodolite and EDM.

Telescope. > Baltery D Telescolop. > Center Mank grip. > vertical motion plate level clamp. D D Do > horizontal Tangen 20 Screw 4 Display + Serial Signal 0 unit Connechon

> components of Total Station.

Scanned with CamScanner

1

Componenti of Total Station
* Right collimation
* an board Battery
* Battary locking Lever.
-X Telescope eye piece
* Telescope focussing knob.
* Telescope grip
* Vertical motional (lamp
* Vertical Tangent Screw.
* Horizontal motion clamp
* horizontal Tangent Screw.
* plate Level
* Instrument Center Maric
* Display Unit
& Serial signal connection.
Type: of Total Station
1. Manual total station
2. Semi automatic
3. Automatic total station.
the second second
* Select a Suitable position for Instrument * Select a Suitable For observer to tation, which is suitable for observer to
ake readings. * Remove the plastic Cap from the
telescope tripod.

- -* Instrument Height is an important aspect for effective and comfortable surveying process
- * level up the total station to an Arbitany point.
- * To occupy the existing Station above reference point first Roughy Level up the tripod. head right above the point.
- * For Levelling up the circular bubble attached to the level is useful.

levelling up

21125

- * adjust the three foot screws to make Level the instrument
 - * after levelling measure the Height of the instrument from the center marked point on the side of the Instrument to the ground and note that value of HI

pre la sionie to be taken during Total Station surveying

* Do not make the total station wet.

* Take maximum care while remared Battery and data tool from the total station.

- * Never Release the handle Before total station is Fixed on it
- & Use Both hands to hold total station @ every time.
- * DO not Carry tripod without Remaring Total Station.
- * Don't choose hot climate for Jotal
- Station work. * Because climate may Influence in Results and errors may occurring during those kind of activities.

Advantages: -* avice setting of the instrument on the tripod using laser plumont.

* ploking and area computation at any user required scale can be done.

* Using Robotic total station Single Surveyor Can perform the whole survey works

* Integration of Data is possible & lasy to arrive Result.

* Automation of world maps and full Gis map creation is possible. Dis advantages * Instrument is costly * Skilled personi Required to perform surveying work's * field check is not possible. * Result Depending upon climatic cond ition's an anadada in te ng en lessartes, di 15 perior a. there and the control largest Verb 10 acoulty and the prophed talk tan b doorp

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